



Example of Total Project Planning – Case Study 2: “Geo-Structures”

*Andreas-Gerasimos Gavras, Ph.D. Student
University of California, Davis
December 14, 2015*



Example of Total Project Planning – Case Study 2: “Geo-Structures”

➤ Objectives

- *This is not a technical research presentation!*
- *Share my experience with large-scale testing at UC San Diego using the Large Soil Confinement Box (LSCB) to study a dynamic soil-structure interaction problem*

➤ Potential Outcomes

- *If you already have a specific test in mind, you might now know something more about the specific steps involved in designing, constructing and testing your idea, and the various decisions you have to make*
- *If you don't have a specific test in mind, perhaps you will become more aware about the facility's capabilities to envision new tests*

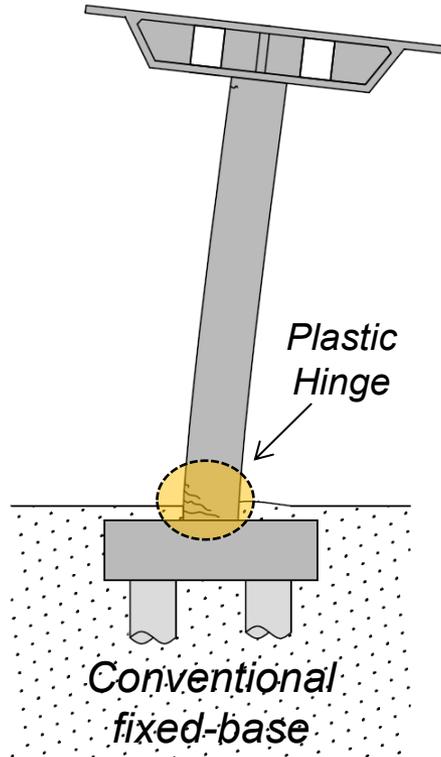
Outline

- ***Project Description***
- ***Test Design***
- ***Experiment Assembly and Construction***
- ***Material Testing***
- ***Instrumentation***
- ***Seismic Testing Protocol***
- ***Test Response***
- ***Concluding Remarks***

Project Description

Project Description

➤ *Rocking Foundations as an Earthquake Damage Resistant Mechanism*



Project Description

- **Why Large-scale 1g Testing of Rocking Foundations at UCSD?**
 - Both large-scale 1g and centrifuge testing do not come without shortcomings
 - Confirm findings from previous centrifuge tests. Will they be different at large-scale?
 - Examine response at large rotations / drift ratios
- **We also wanted to study**
 - Effect of ground water table proximity to the rocking footing
 - Non-planar rocking response
 - (Rocking piled foundations)

Test Type	1g			Centrifuge
	Full-scale	Large-scale	Small-scale	Reduced-scale
Testing frequency of geo-structural systems				
General scaling laws				
Relative scaling of soil particles				
Realistic soil construction				
Realistic superstructural material				
Cost				
Previous tests on rocking foundations				

Project Description

- **“Analytical and Experimental Development of Bridges with Foundations Allowed to Uplift During Earthquakes”**
 - *Award Amount: \$741,479 (50% spent for the experiment)*
 - *Funding: California Department of Transportation (Caltrans)*
 - *Period of Contract: February 2013 – July 2015*
- **Project Components**
 - **Experimental response of single bridge columns**
 - **Numerical modeling validation for single bridge columns**
 - **Parametric study of single bridge columns**
 - **System-level analysis of two realistic, archetype bridges**
 - **Displacement-based design method and guidelines for single bridge columns and bridge systems**

Project Description

➤ **Project Team**

- *Principal Investigators*

- ✓ *Marios A. Panagiotou (formerly UC Berkeley)*
- ✓ *Bruce L. Kutter (UC Davis)*
- ✓ *Jose I. Restrepo (UC San Diego)*
- ✓ *Patrick J. Fox (formely UC San Diego)*
- ✓ *Stephen Mahin (UC Berkeley)*

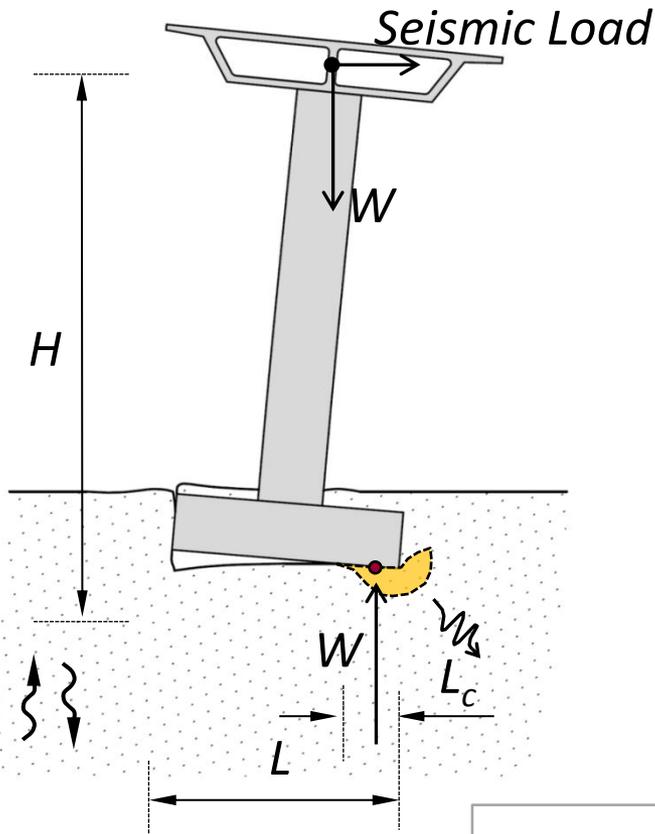
- *Graduate Student Researchers*

- ✓ *Grigorios Antonellis (formerly UC Berkeley)*
- ✓ *Andreas-Gerasimos Gavras (UC Davis)*
- ✓ *Gabriele Guerrini (formerly UC San Diego)*
- ✓ *Andrew C. Sander (UC San Diego)*

Test Design

Test Design

➤ Rocking Foundations' Response Controlling Parameters



Controlling Parameters

- **Normalized-moment-to-shear ratio, H / L**
 - ✓ Rocking vs. sliding and moment-to-shear coupling
 - ✓ $H / L > 1.5$ indicates rocking-dominated response
- **Critical contact area ratio, A / A_c**
 - ✓ Recentering vs. energy dissipation, residual rotations and settlements
 - ✓ $A / A_c > 8$ to minimize settlement
- **Rocking base strength ratio, C_r**
 - ✓ Peak rotations and overturning stability
- **Absolute size, H**
 - ✓ Peak rotations and overturning stability for given H / L

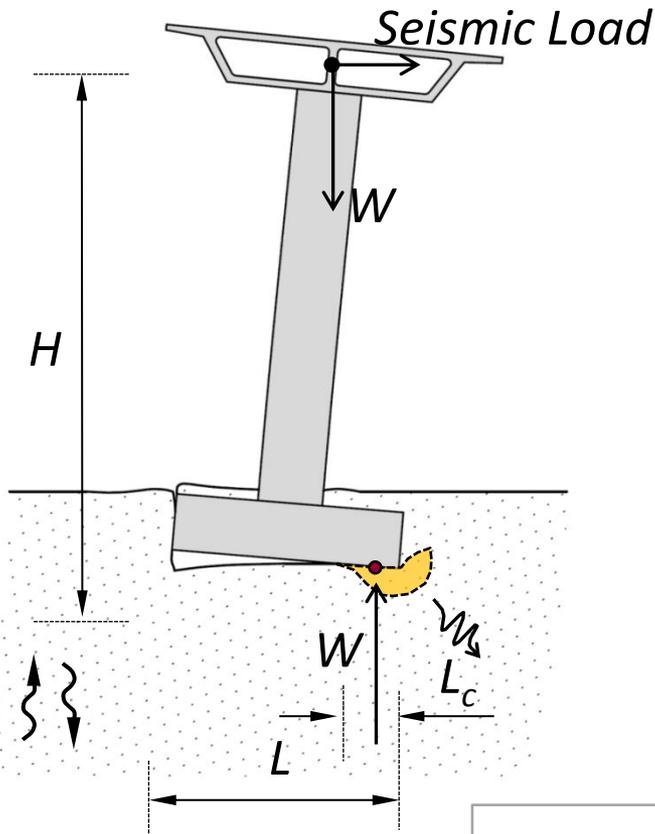
$$\frac{A}{A_c} = \frac{q_c}{q}$$

$$M_{foot} \approx \frac{W \cdot L}{2} \cdot \left(1 - \frac{A_c}{A}\right) + P_p \cdot \frac{D}{3} + k \cdot P_p \cdot \frac{L}{2}$$

$$C_r = \frac{M_{foot}}{H \cdot W}$$

Test Design

➤ Rocking Foundations' Response Controlling Parameters



Prototype vs. Model

For $S_a = 1$, $L_p = S_L \times L_m$ and $W_p = (S_L)^2 \times W_m$

- $L_p \gg L_m$
- $(H/L)_p = (H/L)_m$ (correct scaling)
- $q_p = q_m$
- $(q_c)_p \gg (q_c)_m$ (due to strong dependency of sand bearing capacity to actual footing size)
- $(A/A_c)_p \gg (A/A_c)_m$ (prototype has significantly better re-centering)
- $(C_r)_p \sim (C_r)_m$ (prototype is slightly stronger statically)

$$\frac{A}{A_c} = \frac{q_c}{q}$$

$$M_{foot} \approx \frac{W \cdot L}{2} \cdot \left(1 - \frac{A_c}{A}\right) + P_p \cdot \frac{D}{3} + k \cdot P_p \cdot \frac{L}{2}$$

$$C_r = \frac{M_{foot}}{H \cdot W}$$

Test Design

➤ Design Approach

- Superstructure

- ✓ Structural 1g scaling laws used as a guidance to design superstructure based on the Restrepo et al. (2010) full-scale bridge column test and the available PEER mass blocks
- ✓ Length scale factor, $S_L = \sqrt{W_{ss_m} / W_{ss_p}} = 1/3$
- ✓ Time scale factor, $S_t = \sqrt{S_L / S_a} = \sqrt{1/3 / 1} = 0.577$

- Rocking foundation

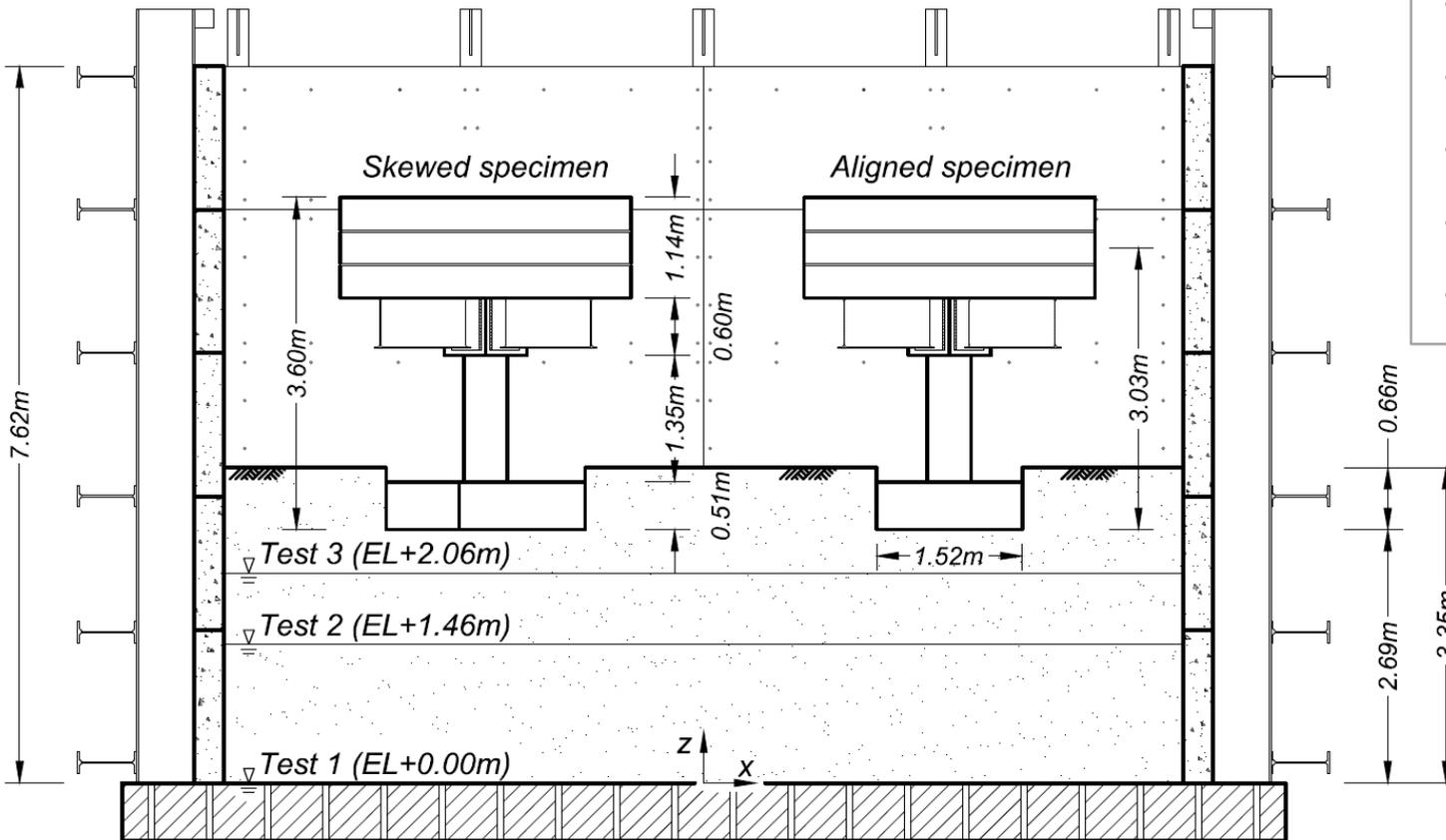
- ✓ Designed directly in model-scale to $C_r = 0.26$, $A / A_c = 8-15$ and $H / L > 1.5$
- ✓ Obtained response is representative of the tested model and not of a prototype

- Soil deposit

- ✓ Sand with target relative density of 80%+ to represent competent soil conditions
- ✓ Sufficiently deep soil profile to minimize boundary effects from the shake table platen

Test Design

➤ Structure and Test Geometry



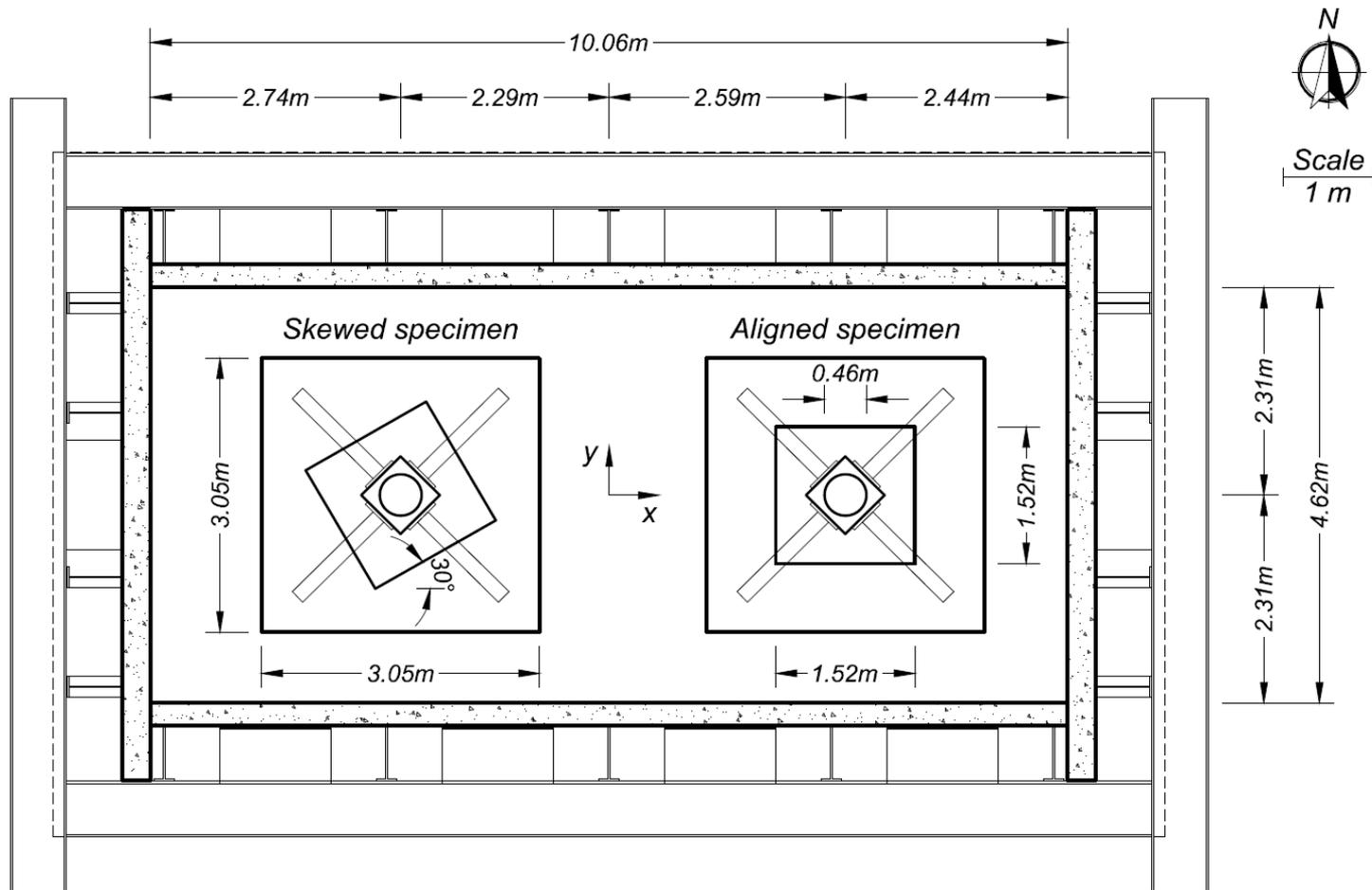
Key parameters

- $W = 290 \text{ kN}$
- $H / L = 2.0$
- $A / A_c = 13$
- $FS_v = 24$
- $C_r = 0.26$
- $C_y = 0.47$

Test Design

➤ Structure and Test Geometry

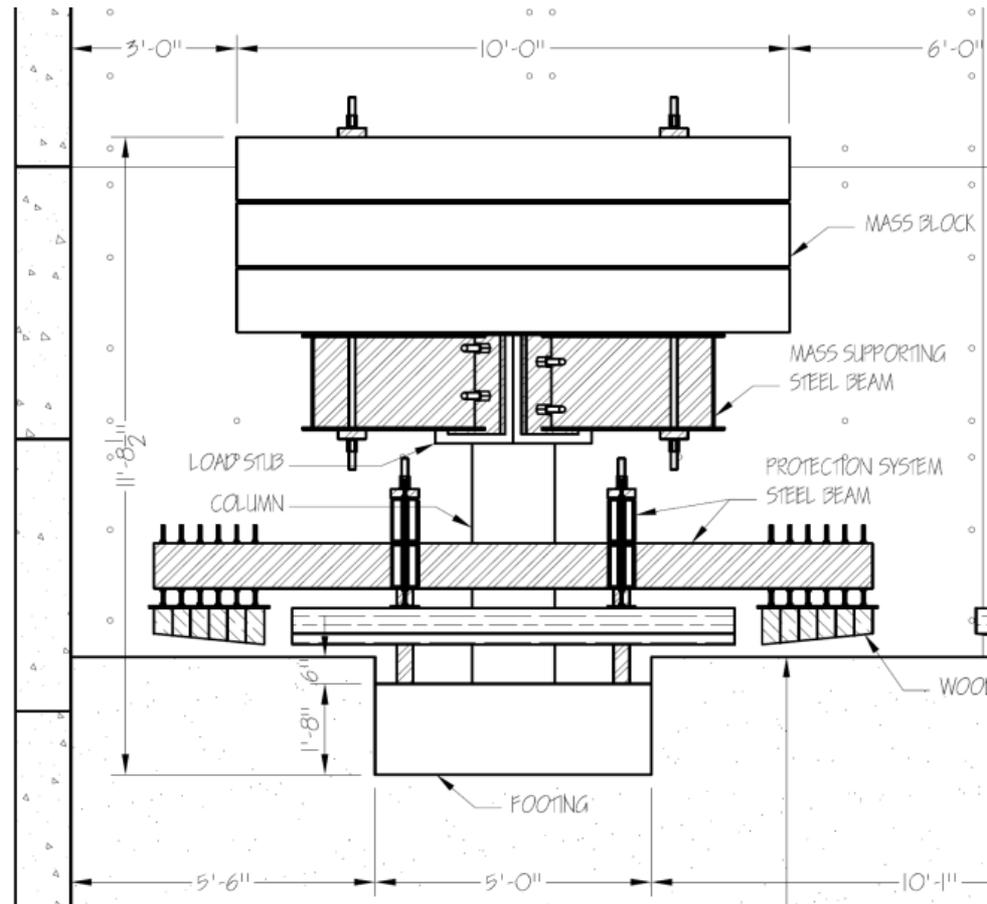
- 2 structures tested concurrently with different footing orientation



Test Design

➤ Restraining System

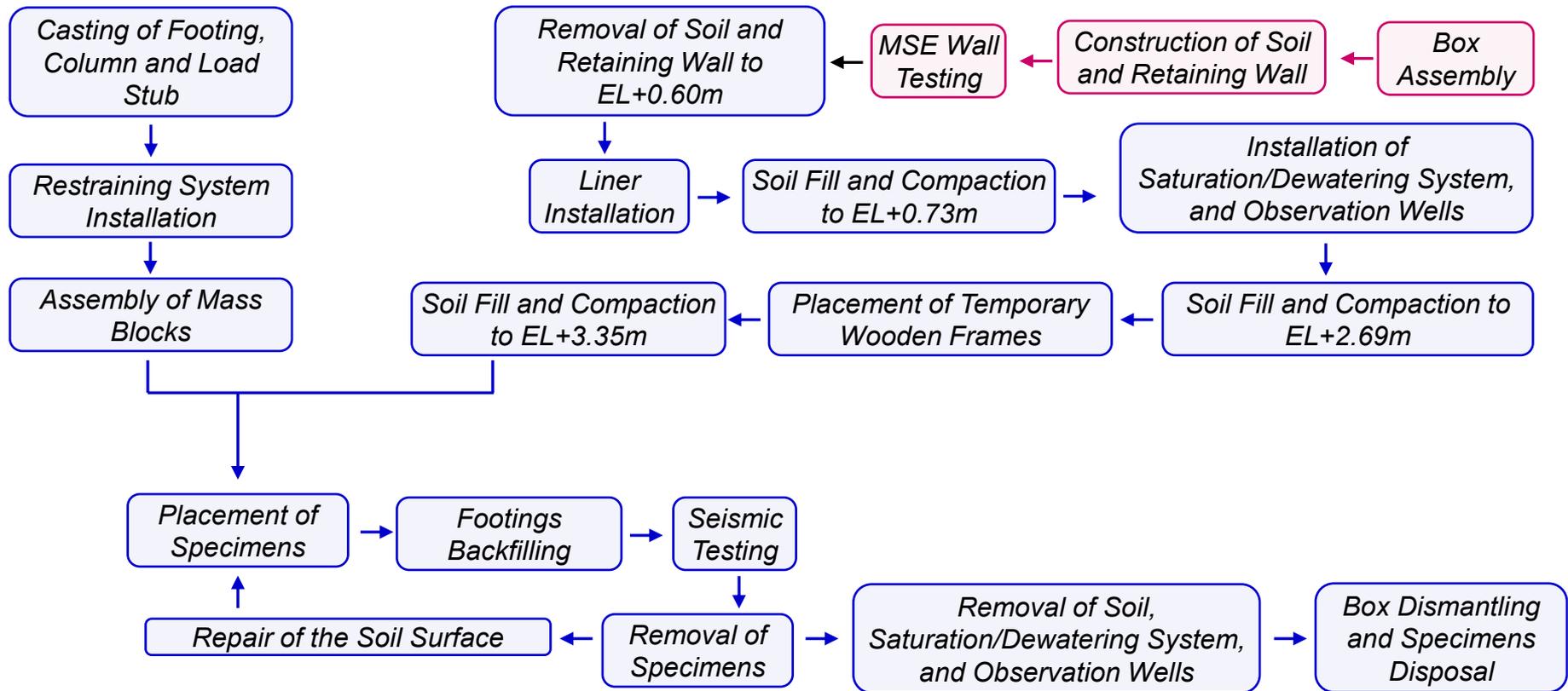
- To prevent overturning and collision of the mass blocks with the box



Experiment Assembly and Construction

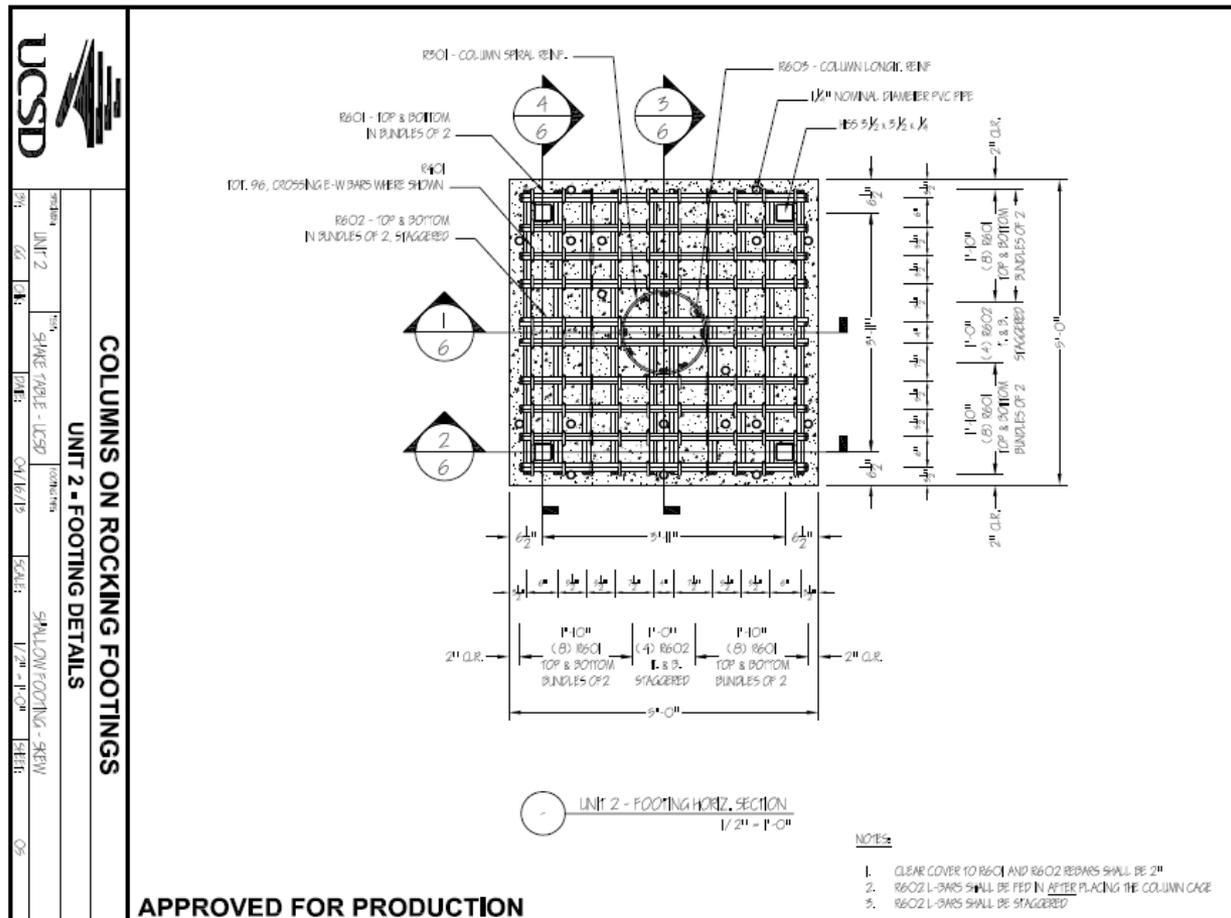
Experiment Assembly and Construction

➤ Simplified Construction Flowchart



Experiment Assembly and Construction

- Casting of footings, columns and load stubs
 - Detailed Construction Drawings



Experiment Assembly and Construction

➤ Casting of footings, columns and load stubs



Experiment Assembly and Construction

➤ Restraining System Assembly



Steel rods and grouting of HSS pipes



Placement of outriggers



Placement of tapered wood beams



Completed restraining system

Experiment Assembly and Construction

➤ Specimens and Restraining System Construction



Placement of mass support steel beams



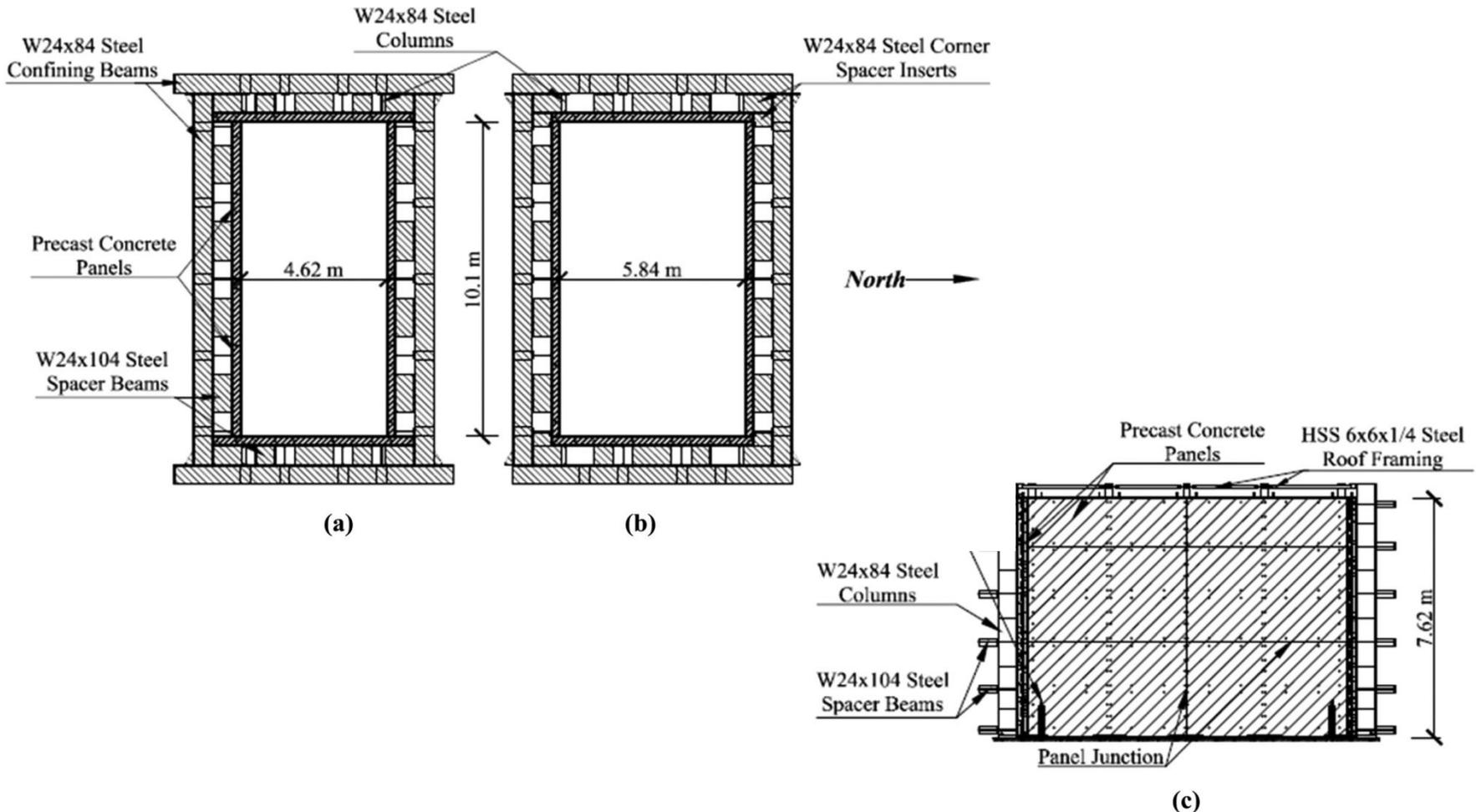
Placement of mass blocks



Completed specimen

Experiment Assembly and Construction

➤ Large Soil Confinement Box



[Source: Fox et al. (2015), Geotechnical Testing Journal]

Experiment Assembly and Construction

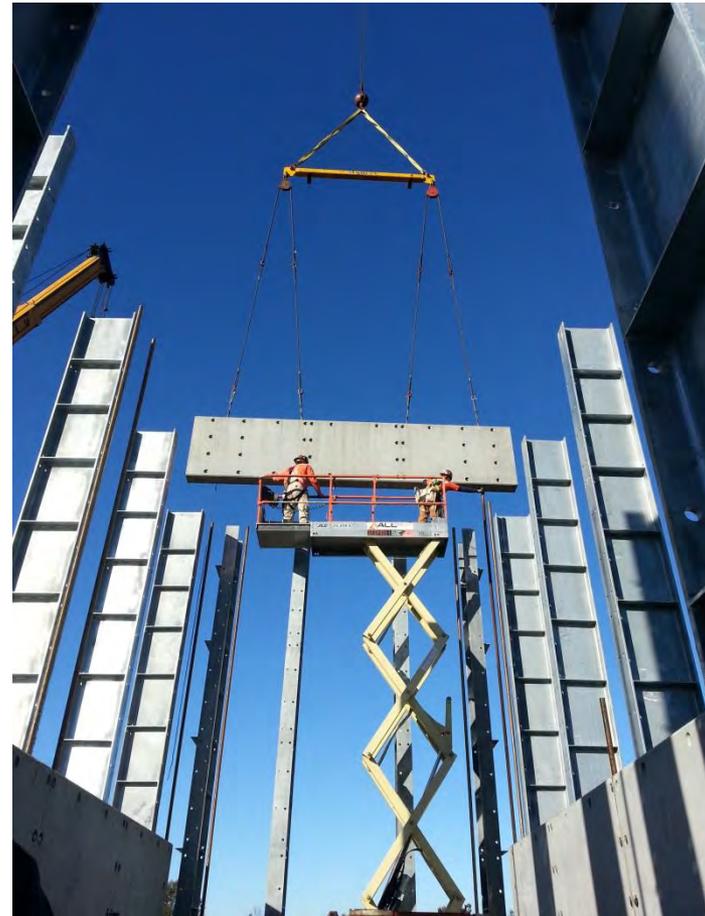
➤ Large Soil Confinement Box

- *Erection of Vertical Elements and Post-Tensioning to the Shake Table Platen*



Experiment Assembly and Construction

- **Large Soil Confinement Box**
 - *Placement of Concrete Panels*



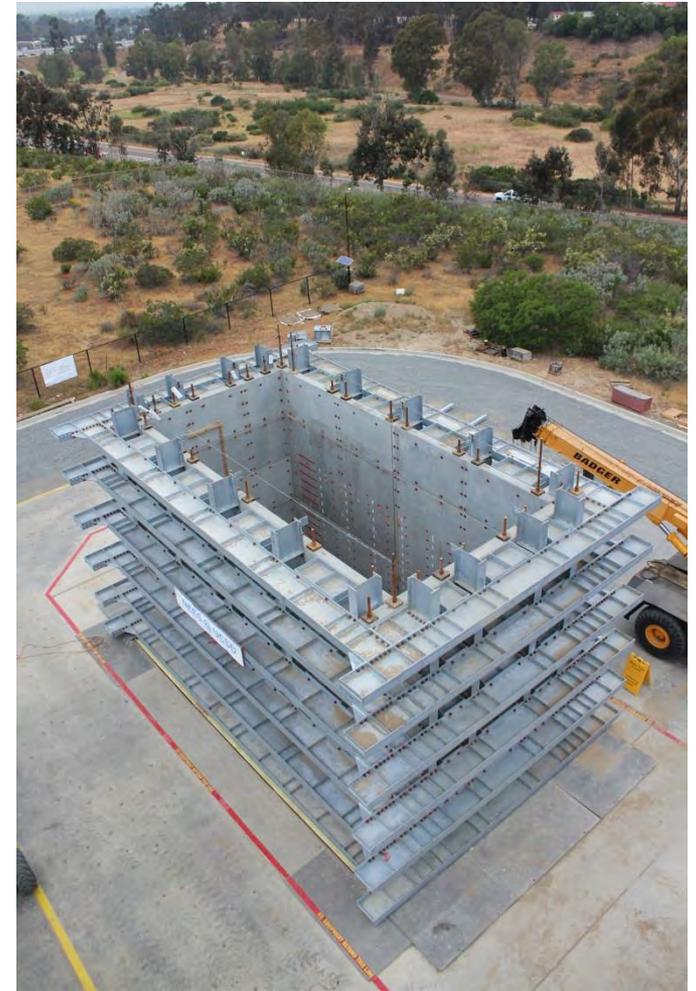
Experiment Assembly and Construction

➤ Time Lapse Video of Assembly



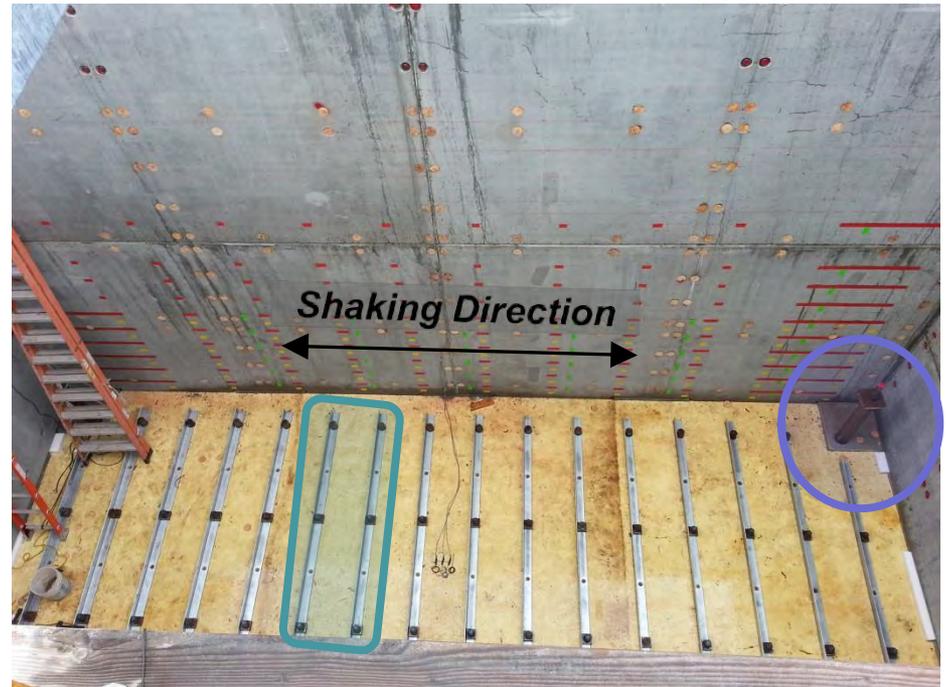
Experiment Assembly and Construction

- **Large Soil Confinement Box**
 - *Exterior Views of Assembled Box*



Experiment Assembly and Construction

- **Large Soil Confinement Box**
 - Interior Views of Assembled Box



16 steel angles bolt to the platen to provide no-slip condition at the bottom boundary

4 PT rods running through the parts of corner column base plates sticking into the box

Experiment Assembly and Construction

➤ Soil Filling and Removal

- Series of Conveyor Belts
 - ✓ Economic, but slow process



Experiment Assembly and Construction

➤ Soil Filling and Removal

- Use of concrete hoppers/buckets and facility's crane
 - ✓ Faster process, but less economic due to crane usage



Experiment Assembly and Construction

➤ Liner

- *Preparation Before Placement*



Experiment Assembly and Construction

➤ Liner

- Placement and Patching



Experiment Assembly and Construction

➤ Saturation and Dewatering System



Experiment Assembly and Construction

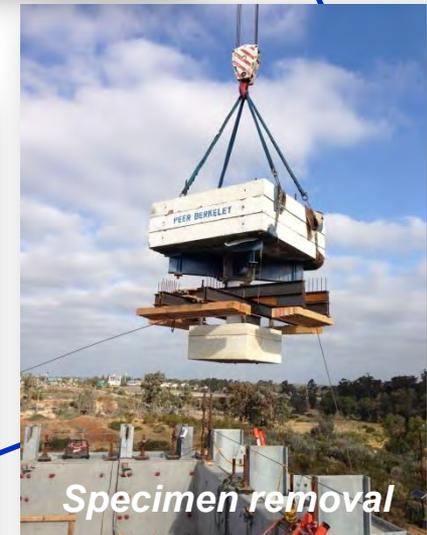
➤ Soil Compaction

- Loose lifts of 200 mm thick compacted at a water content of 6% down to about 150 mm
- Walk-behind vibratory plate with 8 passes per lift
 - ✓ First 4 lifts after placement of liner and saturation/dewatering system
 - ✓ Lifts above the footings' base elevation
 - ✓ Near box walls (in general)
- Skid-steer loader with an attached vibratory roller (1.22 m wide, 7.95 kN heavy vibrating at 40 Hz) with 6 passes per lift



Experiment Assembly and Construction

➤ Testing Cycle

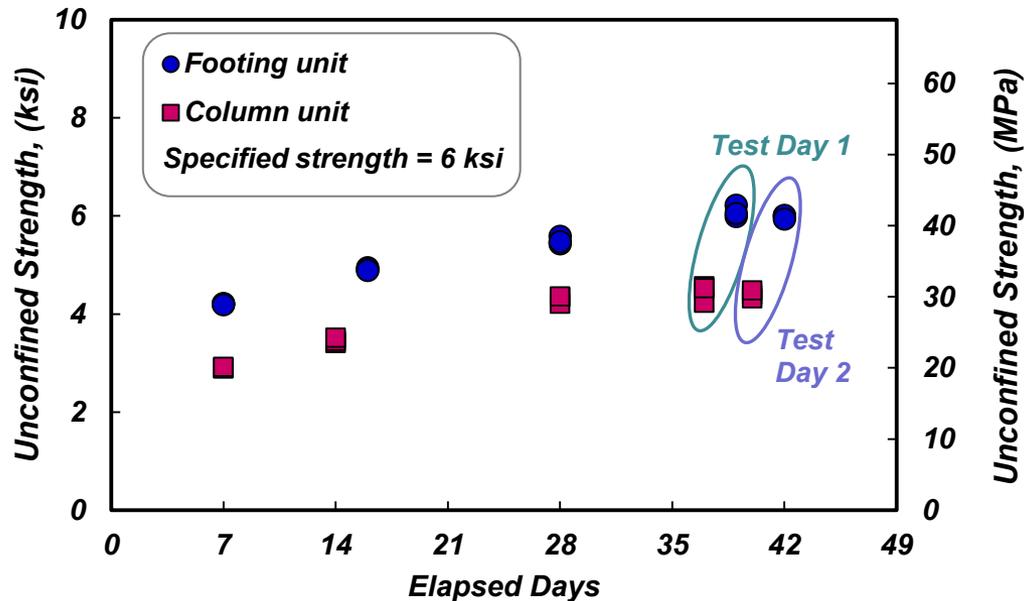


Material Testing

Material Testing

➤ Concrete

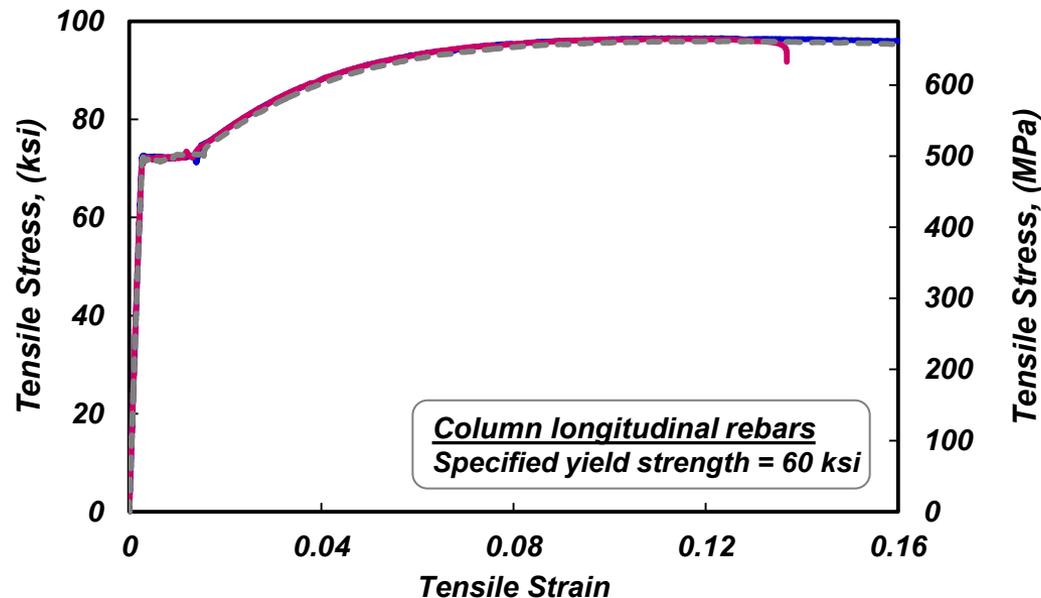
- Slump tests taken prior to casting
- Cylindrical samples taken for UC tests from the footing and column batches to be tested 1, 2, and 4 weeks after casting and at Test Days 1 and 2



Material Testing

➤ Reinforcing Steel

- 3 samples taken for tension tests from each of
 - ✓ Footing main rebars
 - ✓ Column longitudinal rebars
 - ✓ Column spiral
 - ✓ Load stub J-bar stirrups
 - ✓ Load stub staples



Material Testing

➤ Soil Properties Overview

- *Clean, angular, poorly-graded medium sand (ASTM C33 washed concrete sand)*

Classification		SP
Gravel content	[%]	0
Fines content	[%]	2.8
Specific gravity, G_s		2.63
Grain size, D_{50} (D_{10})	[μm]	737 (186)
Coefficient of uniformity, C_u		5.3
Coefficient of curvature, C_c		0.9
Dry unit weight, $\gamma_{d,\min}$ ($\gamma_{d,\max}$)	[kN/m^3]	14.41 (17.72)
Void ratio, e_{\max} (e_{\min})		0.790 (0.456)
Constant-volume friction angle, ϕ_{cv}	[deg.]	≈ 33

Material Testing

- **Considered Methods for Measuring In-situ Relative Density (D_R)**
 - **Sand Cone Test**
 - ✓ *Easy and cheap; can be done by the students*
 - ✓ *Also measures water content*
 - ✓ *High user uncertainty for D_R measurements; can yield scattered results*
 - ✓ *Two measurements possible per day; results available after 24h*
 - **Cone Penetration Test**
 - ✓ *Back-calculates D_R and effective friction angle*
 - ✓ *Needs to be conducted by subcontractors; more expensive, logistic / time issues*
 - **Nuclear Density Gage**
 - ✓ *Accurate measurement of D_R*
 - ✓ *Needs to be conducted by subcontractors; more expensive, logistic / time issues*

Material Testing

➤ Selected Method for Measuring In-situ Relative Density (D_R)

- Sand Cone Test
 - ✓ Logistics and time constraint issues for planned CPT pushes
 - ✓ Consistent compaction protocol with previous project yielding $D_R = 88\%$ based on sand cone tests and nuclear density gage measurements



Material Testing

➤ Sand Cone Test Results

Description	Location			Relative density, D_R (%)	Water content, w (%)
	x (m)	y (m)	z (m)		
Under skew footing center	-2.29	0.30	0.97	86.9	5.1
Under aligned footing center	2.59	0.30	0.97	72.8	4.4
Under skew footing center	-2.29	0.30	1.83	105.7	5.2
Under aligned footing center	2.59	0.30	1.83	95.3	5.7
Under skew footing center	-2.29	0.30	2.49	91.3	3.8
Under aligned footing center	2.59	0.30	2.49	78.4	4.5
Under skew footing center	-2.29	0.00	2.69	68.1	4.9
Under aligned footing center	2.59	0.00	2.69	83.0	4.9
Skew footing backfill before test 1, SE side middle	-1.79	-0.86	3.35	88.6	4.4
Aligned footing backfill before test 1, SE corner	3.58	-0.99	3.35	69.5	3.4
Aligned footing backfill before test 1, S side middle	2.59	-0.99	3.35	95.7	3.2
Skew footing center before test 3	-2.29	0.00	2.69	64.5	5.5
Aligned footing center before test 3	2.59	0.00	2.69	86.9	5.8

Interpreted achieved average relative density, $D_R \approx 90\%$

Instrumentation

Instrumentation

➤ **General Considerations**

- *Must consider available facility instrumentation in advance, and the need to purchase/fabricate sensors specific to your test*
 - ✓ *Pore Pressure Transducers (PPT) to monitor pore pressure build-up in saturated soil*
 - ✓ *Custom-made gap sensors to monitor dynamic evolution of the soil surface under the footings*
- *Clear instrumentation drawings and list of sensors distributed to data acquisition and video personnel before start of construction*
- *Understand construction and instrumentation placement time constraints – coordinate with data acquisition personnel*
 - ✓ *What instrumentation is essential to my test?*
 - *No strain gage installation for the columns*
 - ✓ *What is reasonable instrumentation redundancy?*
 - *Installed sensors = 137; initially proposed = 221*

Instrumentation

➤ Sensors Summary

Sensor	Location	No.	Notes
Accelerometers	Table	3	
	Box	4 (8)	
	Soil, free-field	10	
	Soil, under footings	6 + 8	
	Footings	7 + 8	
	Protection system	(1+2)	
	Mass blocks	8 + 8	
Total	76		
String Potentiometers	Mass blocks	6 + 6	(4) 10in, (6) 25in, (2) 50in
	Footings	6 + 6	(5) 5in, (7) 20in
	Soil settlement	4 + 5	(9) 5in
	Total	33	(14) 5in, (4) 10in, (7) 20in, (6) 25in, (2) 50in
Linear Potentiometers	Gap/no gap	10 + 10	(20) 50mm
	Total	20	(20) 50mm
Pore Pressure Transducers	Soil, free-field	4	
	Soil, under footings	2 + 2	
	Total	8	
Total No. of Sensors		137	

Sensor	Location	No.	Notes
Accelerometers	Table	3	
	Box	4 (8)	
	Soil, free-field	10	
	Soil, under footings	8 + 9	
	Footings	7 + 8	
	Protection system	(1+2)	
	Mass blocks	8 + 8	
Total	76		
String Potentiometers	Mass blocks	6 + 6	(4) 10in, (6) 25in, (2) 50in
	Footings	6 + 6	(5) 5in, (7) 20in
	Soil settlement	4 + 5	(9) 5in
	Total	33	(14) 5in, (4) 10in, (7) 20in, (6) 25in, (2) 50in
Linear Potentiometers	Gap/no gap	10 + 10	(20) 50mm
	Total	20	(20) 50mm
Pore Pressure Transducers	Soil, free-field	4	
	Soil, under footings	2 + 2	
	Total	8	
Total No. of Sensors		137	

Instrumentation

➤ Sensors Nomenclature

A: Accelerometers					
B: Soil	F: Free-field	S: South position in S-N plane	E: East position in E-W plane	S: South orientation	0: Reference EL+0'-0"
F: Footing	Z: Under/at straight footing/specimen	M: Middle position in S-N plane	M: Middle position in E-W plane	N: North orientation	1: EL+3'-0"
M: Mass base	T: Under/at skewed footing specimens	N: North position in S-N plane	W: West position in E-W plane	E: East orientation	2: EL+6'-0"
T: Table			W: West orientation	S: EL+8'-7"	
B: Box			U: Upwards orientation	4: EL+8'-10"	

S: String Potentiometers		LP: Linear Potentiometers	
F: Footing	Z: Under/at straight footing/specimen	S: South position in S-N plane	E: East position in E-W plane
M: Mass base	T: Under/at skewed footing specimens	M: Middle position in S-N plane	M: Middle position in E-W plane
S: Soil		N: North position in S-N plane	W: West position in E-W plane
G: Gap - no gap			U: Upwards orientation
			D: Downwards orientation

PP: Pore Pressure Transducers			
F: Free-field	S: South position in S-N plane	E: East position in E-W plane	1: EL+3'-0"
Z: Under/at straight footing/specimen	M: Middle position in S-N plane	M: Middle position in E-W plane	2: EL+6'-0"
T: Under/at skewed footing specimens	N: North position in S-N plane	W: West position in E-W plane	

AC: Correction Accelerometers			
P: Protection system	Z/T: At angle/skewed footing specimens	S: South orientation	
B: Box	E/W/N/S: East/West/North/South	N: North orientation	
		E: East orientation	
		W: West orientation	
		U: Upwards orientation	
		D: Downwards orientation	

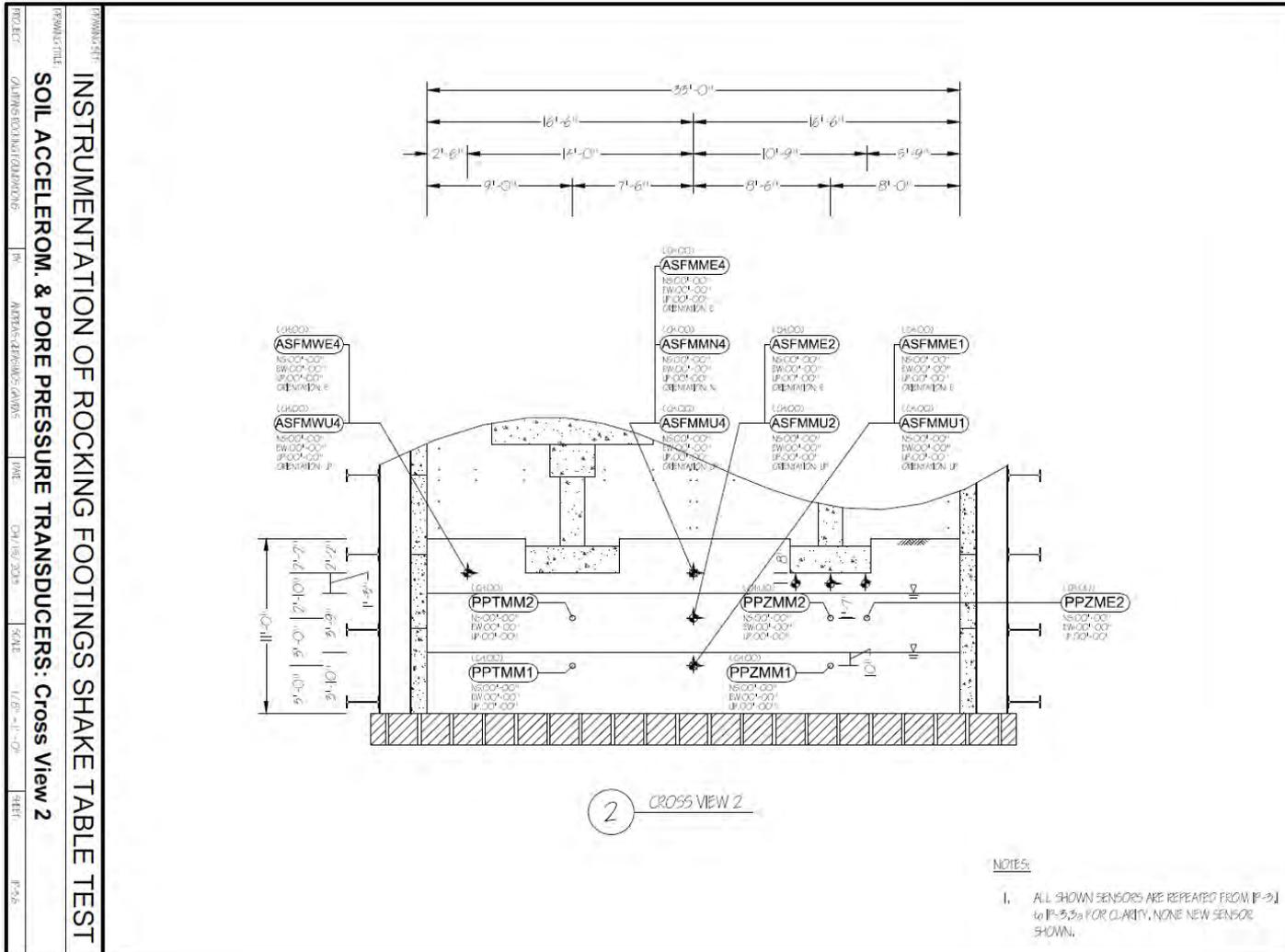
INSTRUMENTATION OF ROCKING FOOTINGS SHAKE TABLE TEST					
Sensors Description					
Model No.					
Manufacturer					

A: Accelerometers

S: Soil	F: Free-field	S: South position in S-N plane	E: East position in E-W plane	S: South orientation	0: Reference EL+0'-0"
F: Footing	Z: Under/at straight footing/specimen	M: Middle position in S-N plane	M: Middle position in E-W plane	N: North orientation	1: EL+3'-0"
M: Mass block	T: Under/at skewed footing specimens	N: North position in S-N plane	W: West position in E-W plane	E: East orientation	2: EL+6'-0"
T: Table				W: West orientation	3: EL+8'-7"
B: Box				U: Upwards orientation	4: EL+8'-10"

Instrumentation

➤ Soil Instrumentation Drawings



Instrumentation

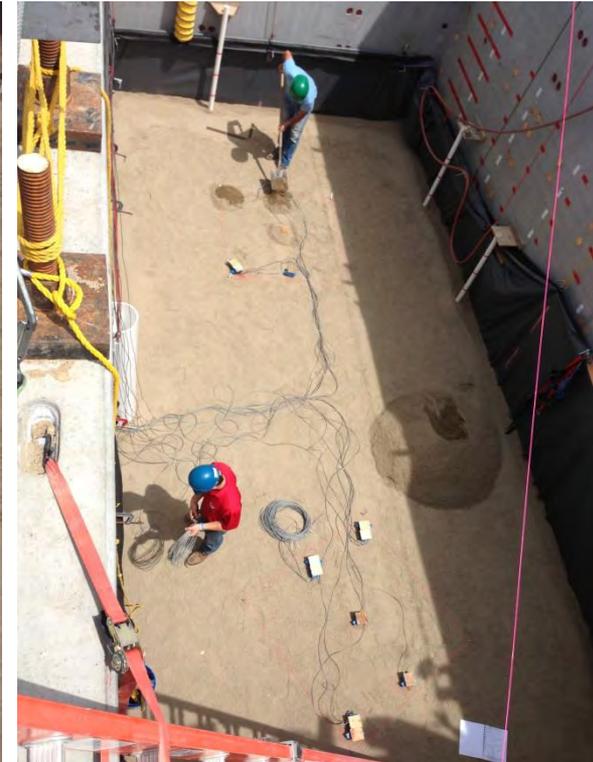
➤ Soil Accelerometers Placement



Marking of locations before placement



Placement of accelerometers



Covering with soil and cables running

Instrumentation

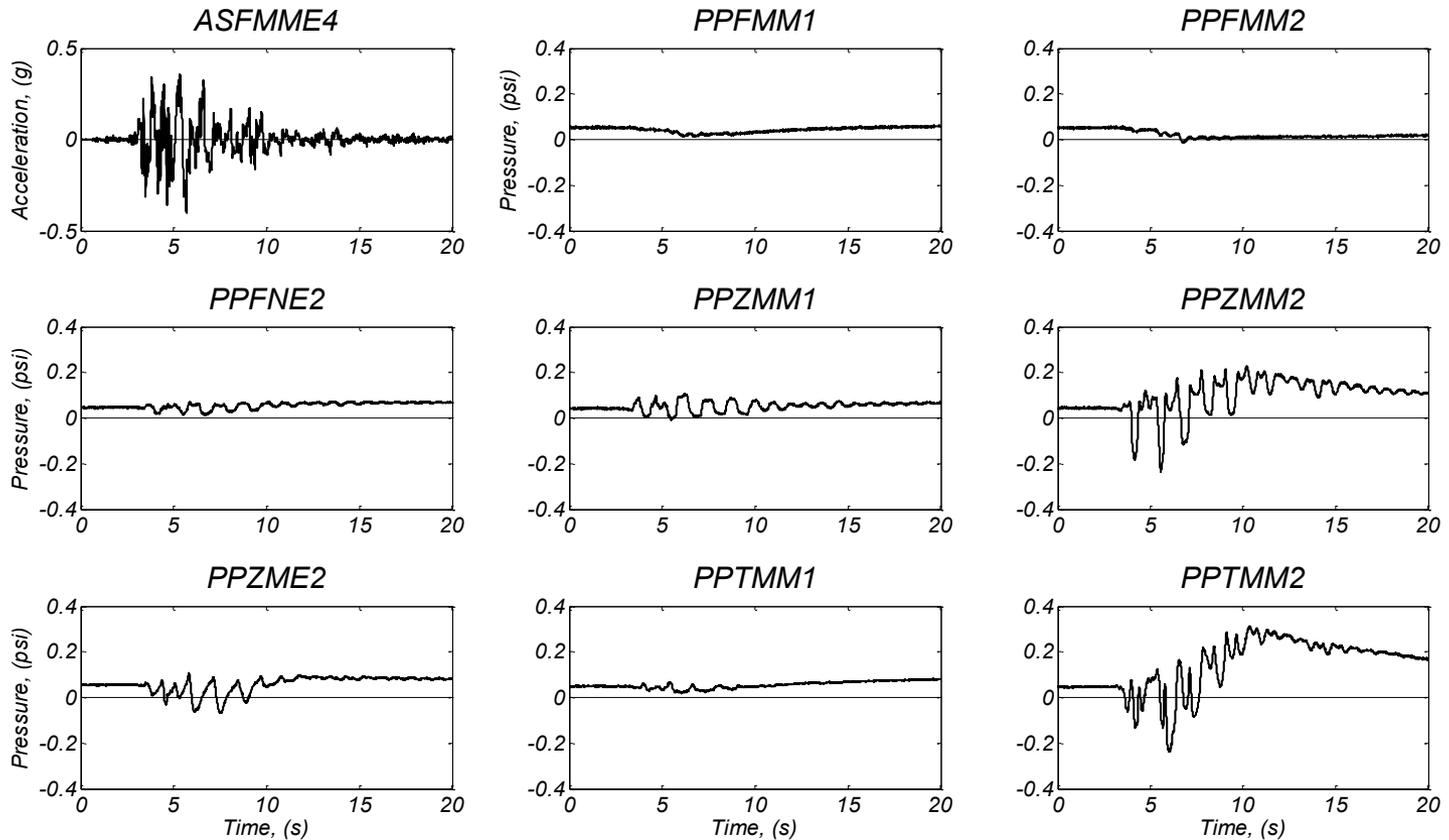
➤ Pore Pressure Transducers (PPT) Placement

- Challenging to prevent desaturation of sensors during the 2-3 weeks period for which they remained above water table



Instrumentation

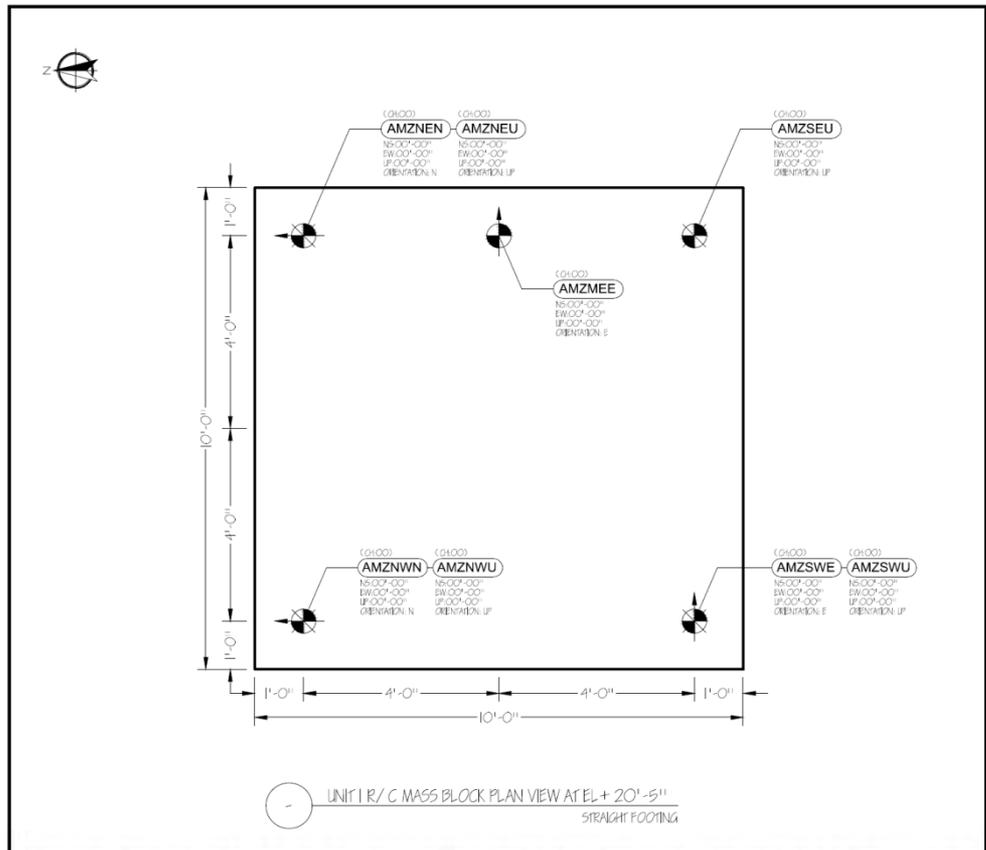
➤ Soil Pore Pressure Response



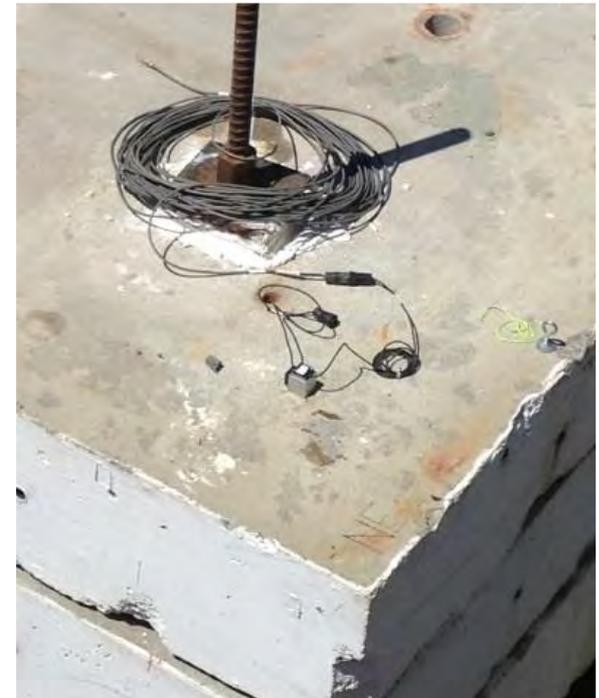
Sensor de-saturation or incomplete soil saturation?

Instrumentation

- Structures' Instrumentation
 - Mass Blocks' Accelerometers



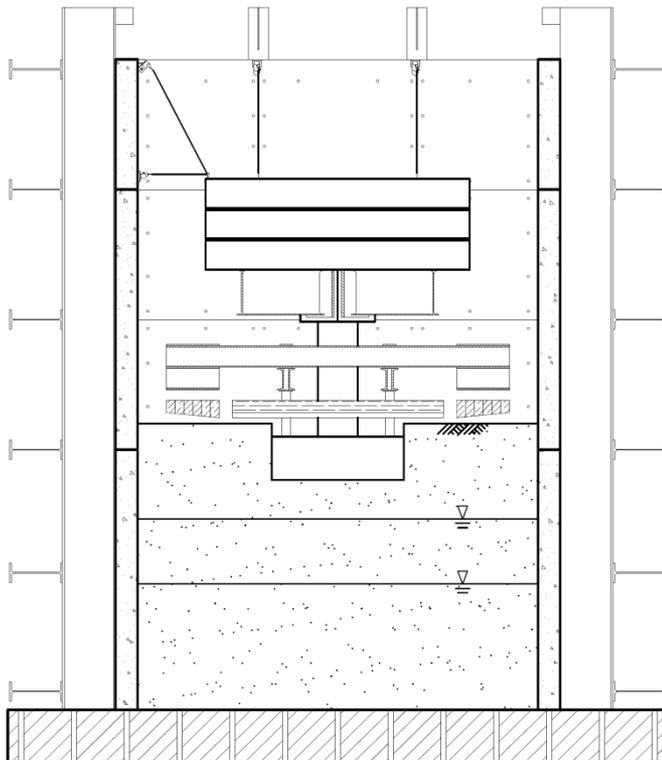
DRAWING SET				INSTRUMENTATION OF ROCKING FOOTINGS SHAKE TABLE TEST			
DRAWING TITLE				SPECIMENS ACCELEROMETERS: Unit 1 Mass Block Plan View			
PROJECT:	CALTRANS ROCKING FOUNDATIONS	BY:	ANITA AS-GONZALEZ/GAVIN AS	DATE:	04/16/2015	SCALE:	3/8" = 1'-0"
						SHEET:	F-4.5



Instrumentation

➤ Structures' Instrumentation

- *Mass Blocks' String Potentiometers*
 - ✓ *6 linearly independent String Pots (3 horizontal + 3 vertical) to determine 6 DoFs*



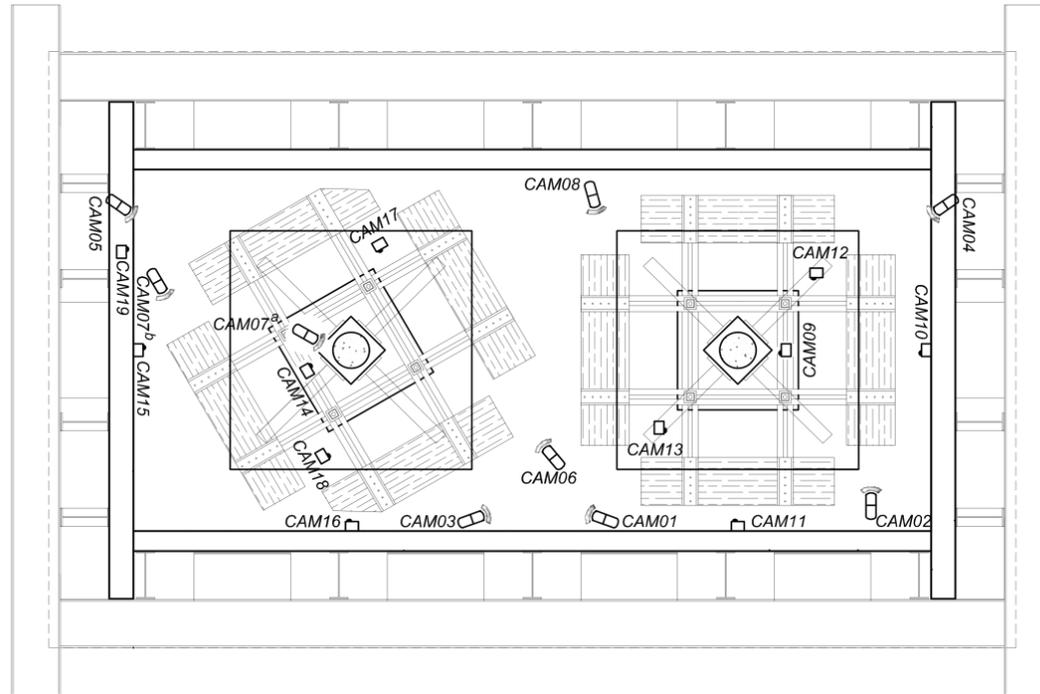
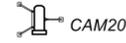
Instrumentation

➤ **Video Cameras Used**

- *Coaxial cameras [8]*
 - ✓ *Wired, power-supported, low resolution (768 × 494 pixels at 30 fps)*
 - ✓ *Live video streaming; can be played back during testing*
 - ✓ *168 out of 168 events successfully recorded*
- *GoPro2 cameras [11]*
 - ✓ *Wireless, battery-supported, high resolution (1920 × 1080 pixels at 30 fps)*
 - ✓ *Can be accessed and played back after testing*
 - ✓ *126 out of 231 events successfully recorded*
- *Sony cameras [2]*
 - ✓ *Man-operated, battery-supported, high resolution (1920 × 1080 pixels at 30 fps)*
 - ✓ *Can be accessed and played back after testing*
 - ✓ *29 out of 42 events successfully recorded*

Instrumentation

➤ Video Cameras Layout



- GoPro3
- Coaxial
- Sony

Instrumentation

➤ Coaxial Cameras Views



Seismic Testing Protocol

Seismic Testing Protocol

➤ **Developing a Motion Protocol**

- *Selection of number of motions and target drift ratios (Θ) for each motion*
 - ✓ *Test days 1 and 2: 6 motions of increasing intensity (peak $\Theta < 13\%$ to avoid mobilization of the restraining system and damage to the column)*
 - ✓ *Test day 3: additional 2-3 motions*
- *Pre-test prediction required to guide selection of motions to match objectives*
- *Comparison of predicted and achieved response after each motion*

➤ **Additional Considerations**

- *Candidate motions need to be selected and distributed to Operations Manager before filling the box with soil to run OLI tests*
 - ✓ *Candidate motions: 9 unique records; 15 in total*
 - ✓ *Used motions: 6 unique records; 9 in total*
- *Peak input acceleration < 0.80 g to ensure LSCB integrity due to removal of the roof framing elements*

Seismic Testing Protocol

➤ Motion Protocol

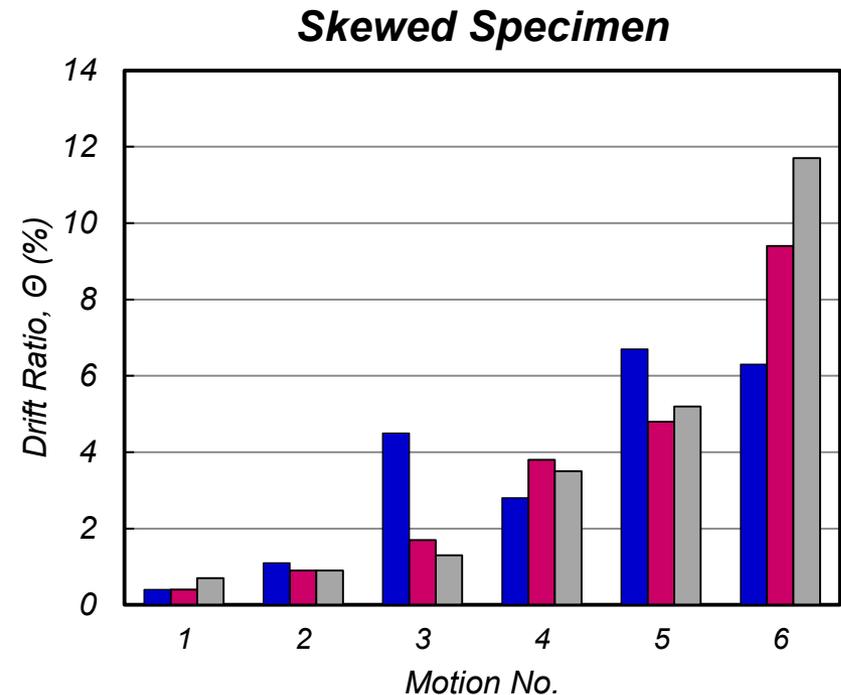
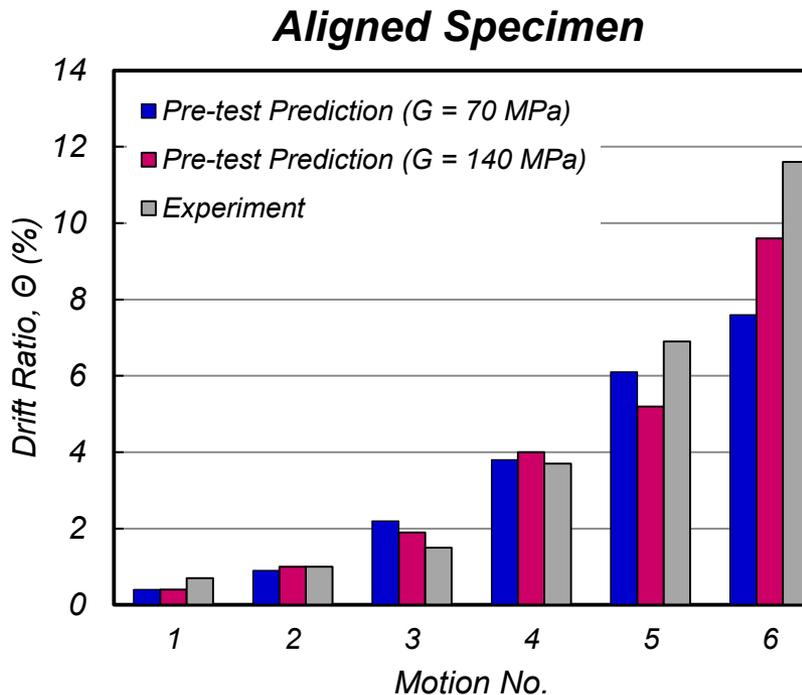
No.	Earthquake	Ground motion	Scale Factor	Target Drift Ratio, θ (%)	PGA, (g)
1	1989 Loma Prieta, CA	Gilroy #1	1.0	<0.5	0.47
2	1989 Loma Prieta, CA	Corralitos	0.8	1	0.39
3	Imperial Valley, CA, 1979	El Centro #6	1.1	2	0.49
4	1971 San Fernando, CA	Pacoima Dam	0.8	4	0.52
5	1995 Kobe, Japan	Takatori	0.5	6	0.34
6	1995 Kobe, Japan	Takatori	1.0	>8	0.68
7	1987 Superstition Hills (B)	Parachute Test Site	1.0	>8	0.42
8	1987 Superstition Hills (B)	Parachute Test Site	-1.0	>8	0.42
9	1987 Superstition Hills (B)	Parachute Test Site	1.1	>8	0.46

Notes

- (1) Motions 7 – 9 only for Test 3.
- (2) White noise with 0.05g RMS amplitude and 5 mins duration applied before motion 1 and after each motion.
- (3) Motions compressed in time by $\sqrt{1/3} = 0.577$.

Seismic Testing Protocol

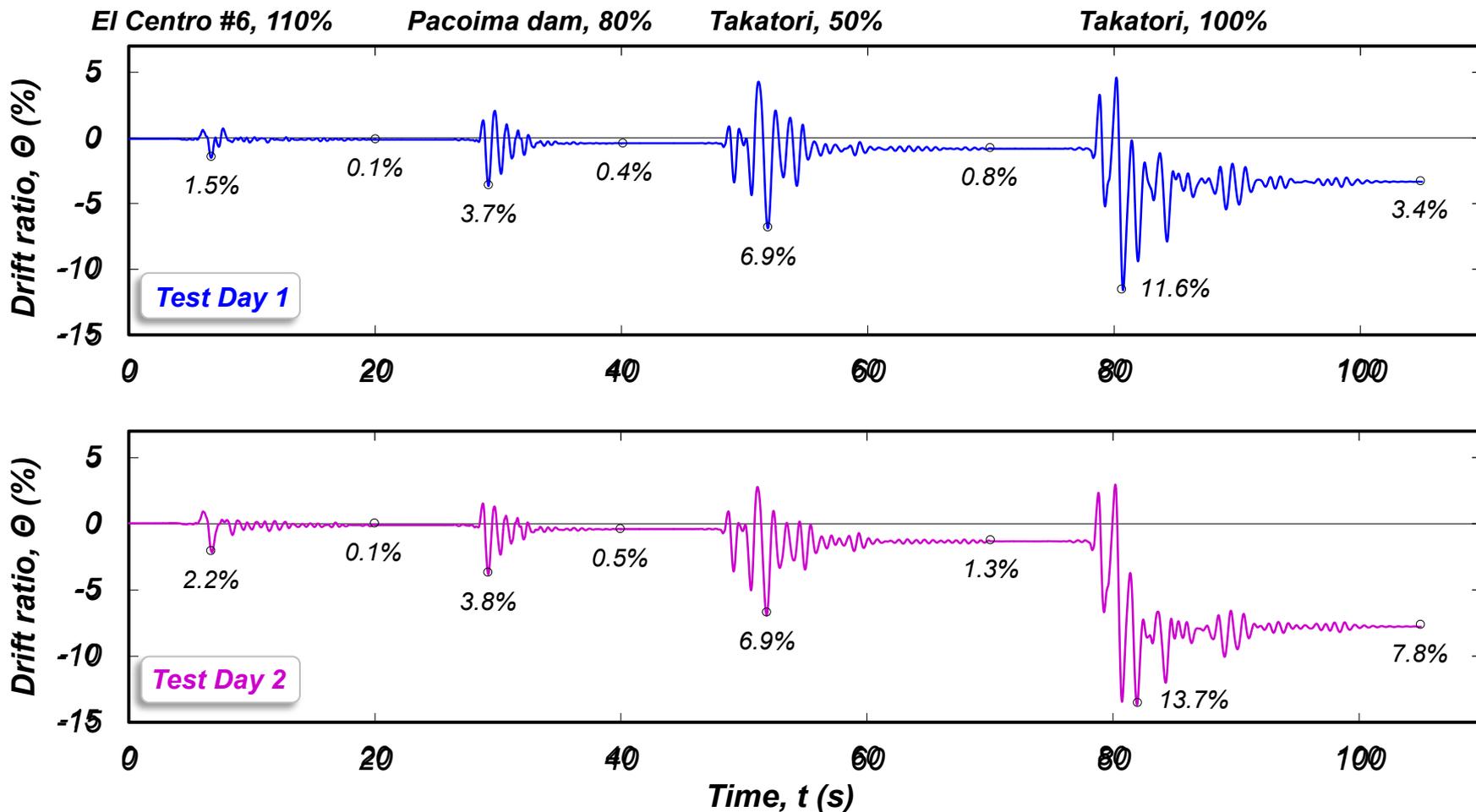
➤ Comparison of Pre-test Prediction with Test Day 1 Results



Test Response

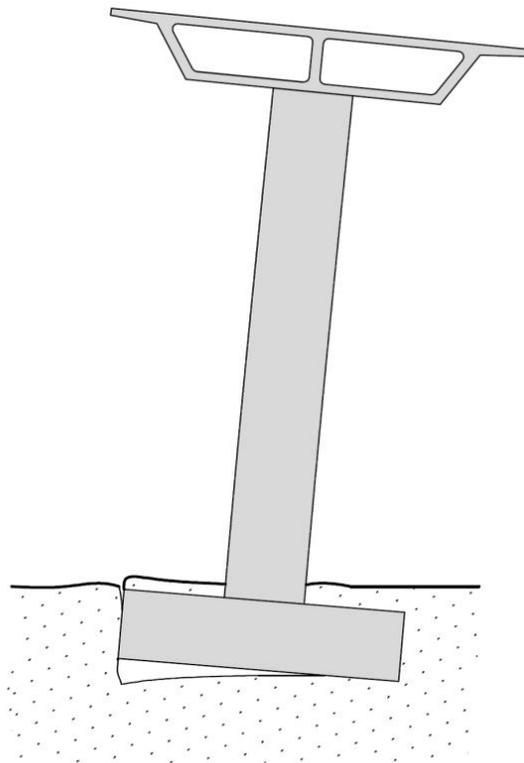
Test Response

➤ Column Drift Ratio Time Histories for Test Days 1 and 2

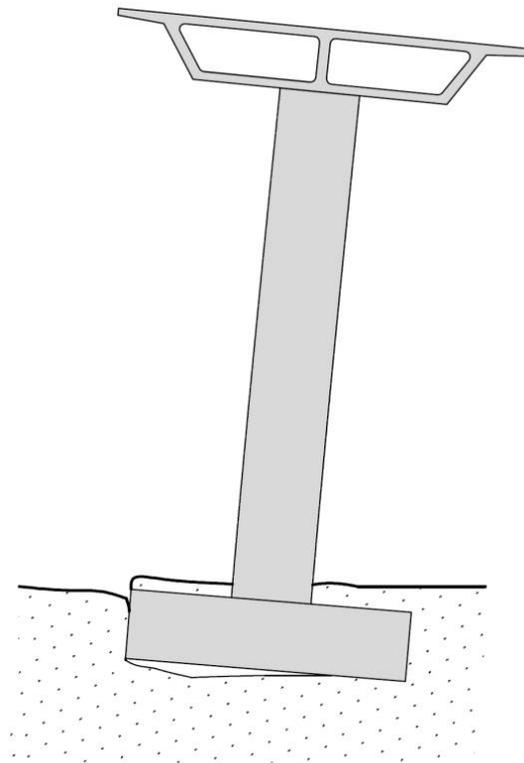


Test Response

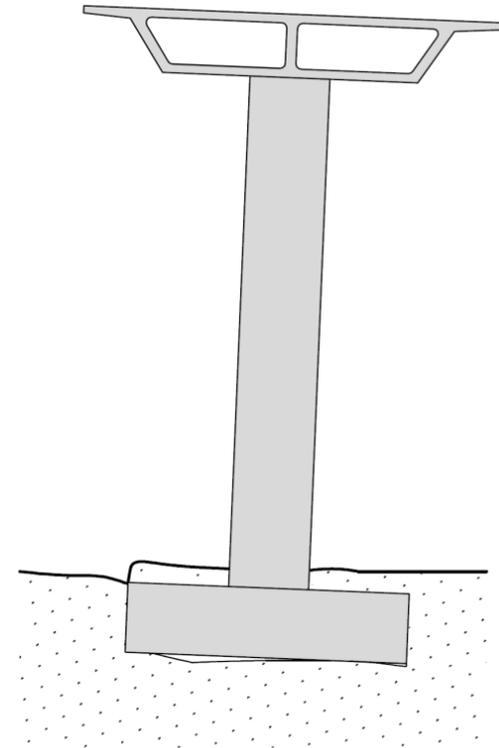
➤ Mechanism for Flow of Sand under the Footing



Gap formation



Sand flowing into the gap



Residual rotation

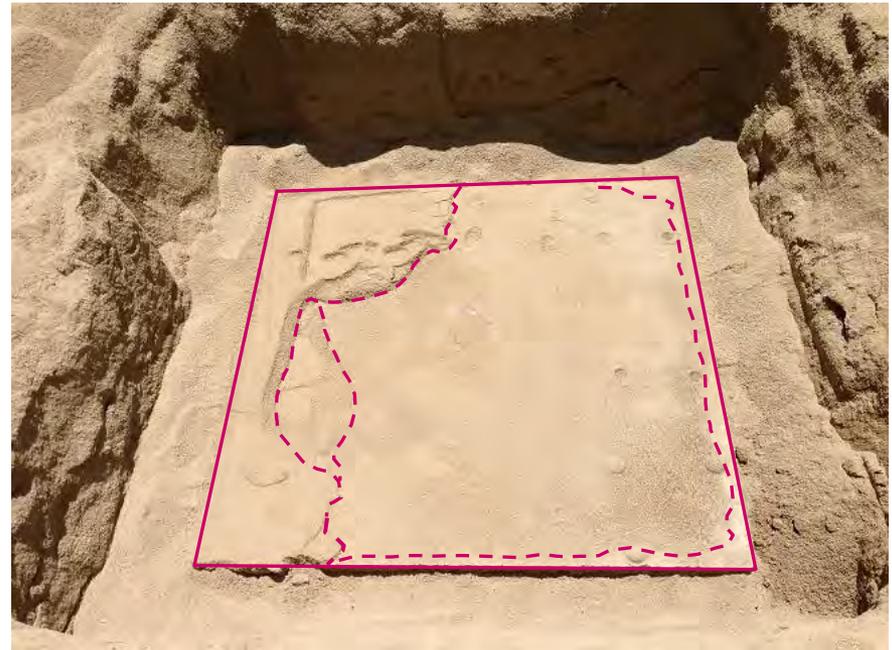
Test Response

➤ Post-test Soil Surface under Footings

Test Day 1

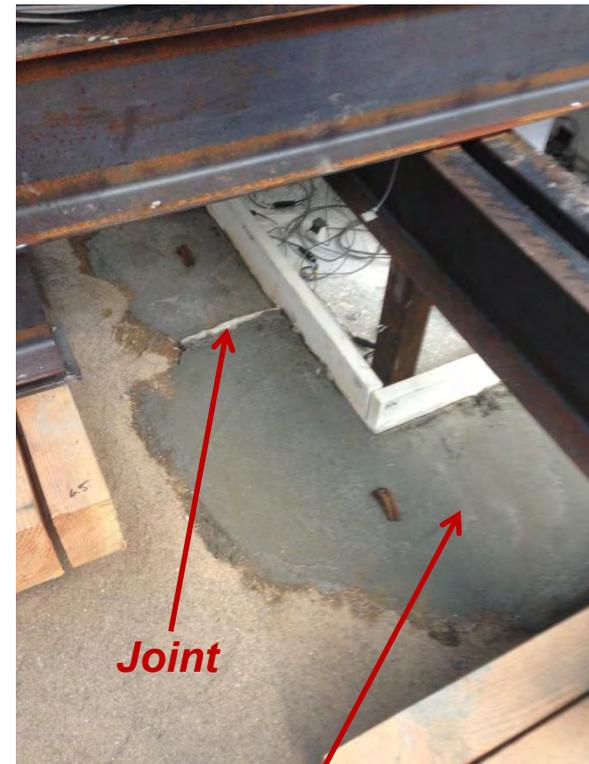
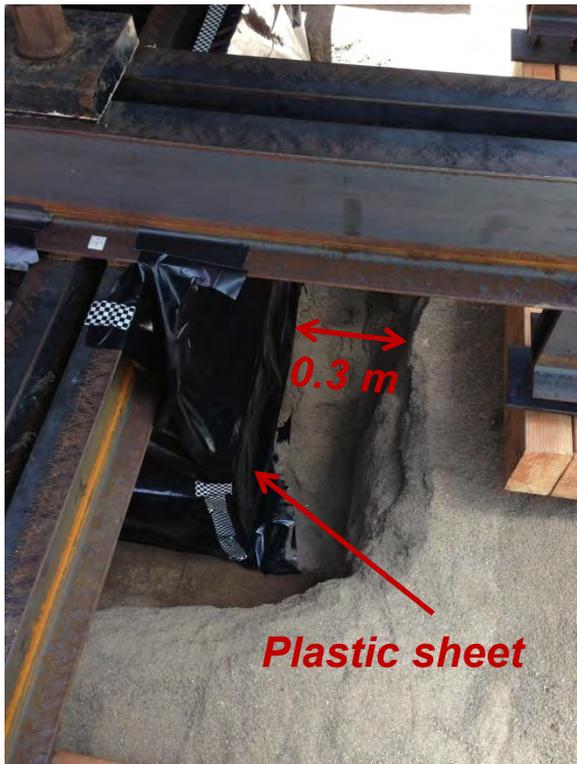


Test Day 2



Test Response

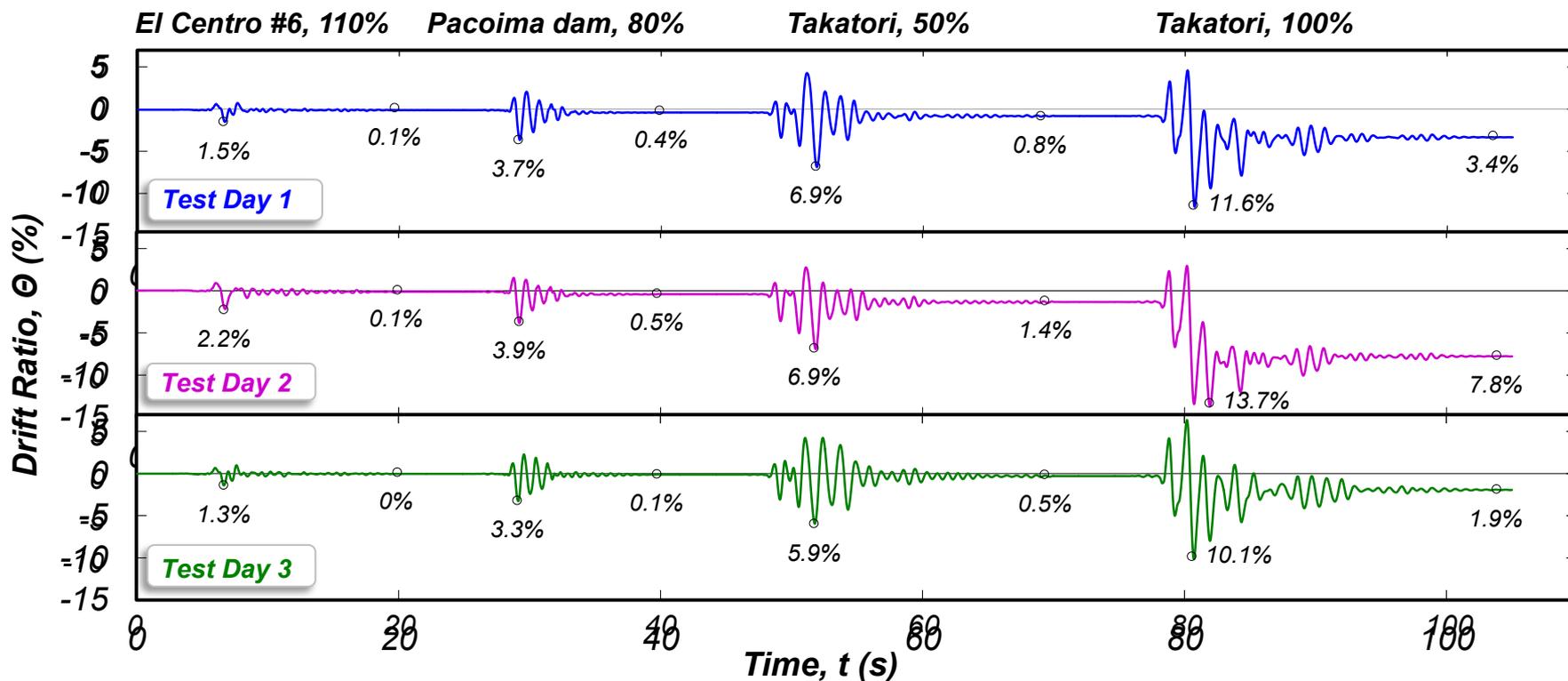
- **Remediation Method for Test Day 3**
 - *Weak Concrete Cast around the Footings*



Concrete, $f'_c \approx 3.5 \text{ MPa}$ [0.5 ksi]
(cast one day before the test)

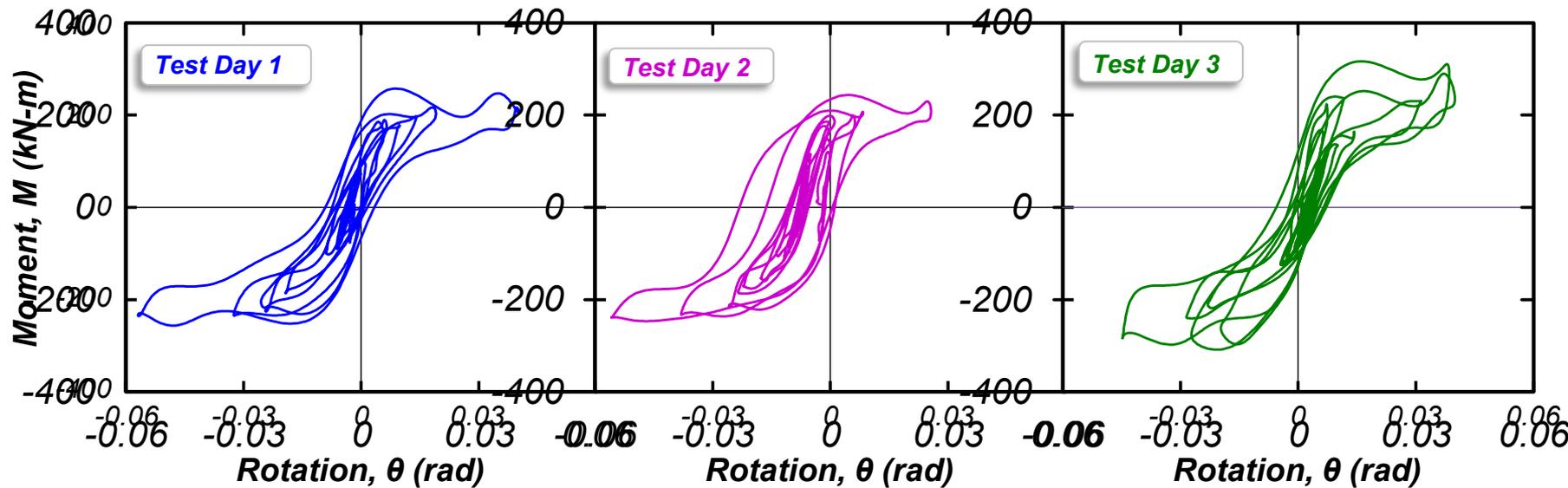
Test Response

➤ Column Drift Ratio Time Histories (revisited)



Test Response

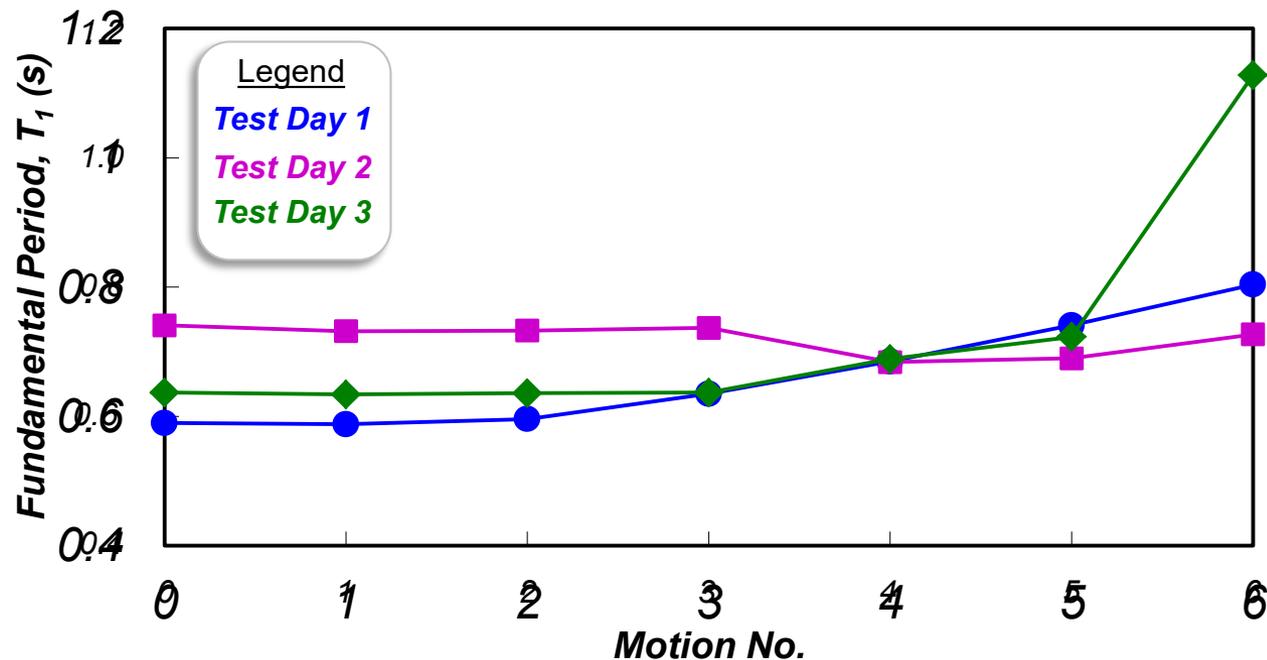
➤ Foundation Hysteretic Response – Takatori, 50%



Test Response

➤ System Softening and Period Elongation

- Determined from white-noise vibrations based on the ARS amplification ratio



Test Response



Cost Disaggregation

Item	Cost	Percentage (%)
Liner, Saturation and Dewatering System	\$2,619	0.7
Pore Pressure Transducers	\$1,719	0.5
Analysis of Soil Box	\$5,737	1.6
Specimens Construction	\$10,502	2.9
Restraining System	\$18,000	4.9
Mass Blocks Shipment	\$7,800	2.1
Box Demolition	\$51,000	13.9
Facility Use	\$101,000	27.5
Facility Labor	\$98,858	26.9
Equipment Renting	\$41,539	11.3
Other Materials	\$28,285	7.7
Total Experimental Cost	\$367,059	100.0

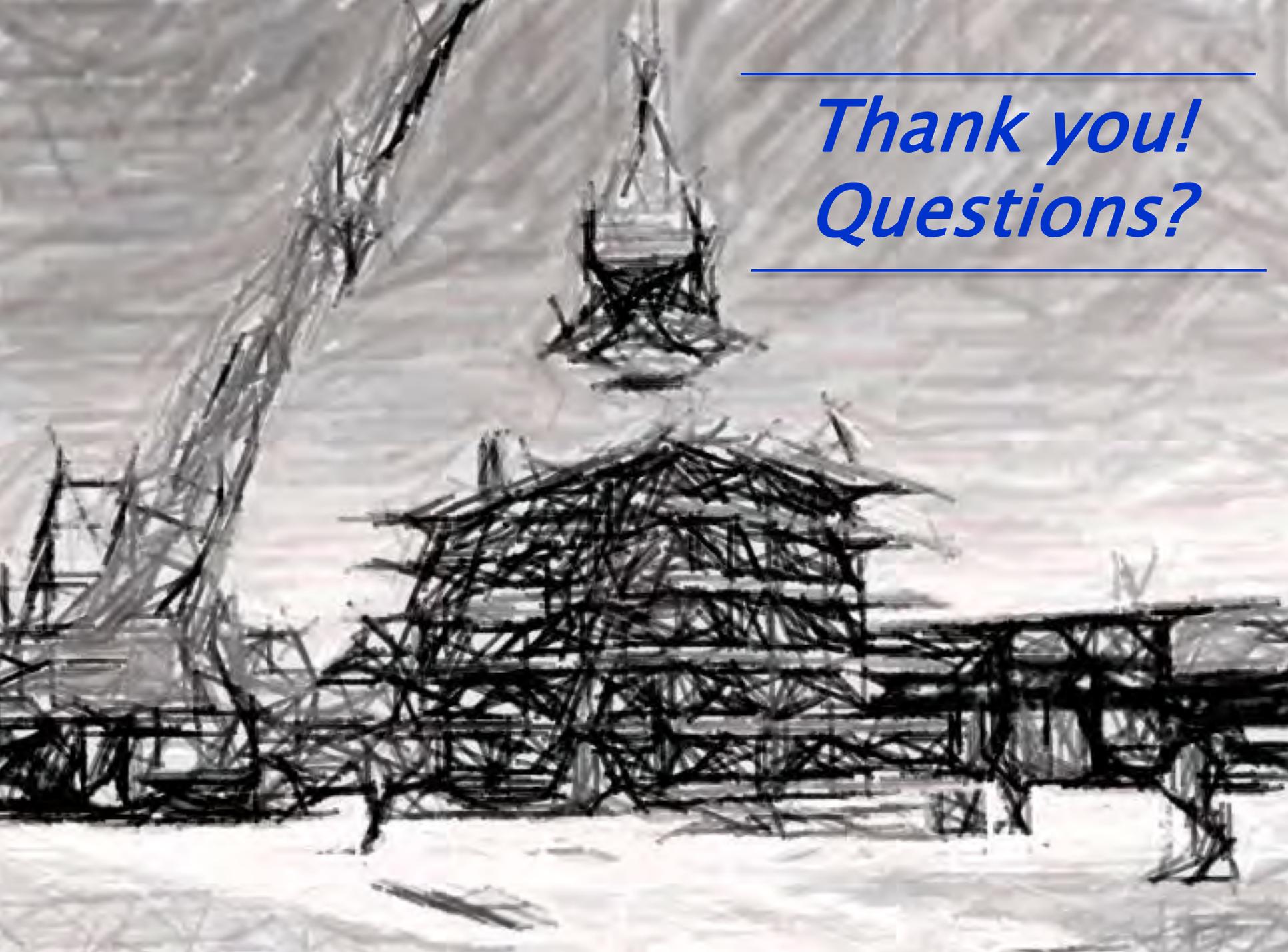
Concluding Remarks

- *This presentation focused on some of the design, construction and testing aspects of a large-scale 1g testing of a geo-structural system at UCSD*
- *Detailed documentation of protocols and detailed preparation of designs increases quality of communication and coordination amongst the various processes*
- *Testing decisions should reflect the target of measuring and gaining insights into specified targeted responses and mechanisms*
- *The efficacy of a physical modeling test of this scale reflects the details of the preparation and execution phases*

Concluding Remarks

- *The test progress is not a straight line. Adjustments should be expected subject to:*
 - *Preliminary results during the design phase*
 - *Gained insights during testing*
 - *Time- and cost-limitations*

Thank you!
Questions?



Acknowledgements

- *Project funded by California Department of Transportation*
- *Principal investigators*
 - *Marios Panagiotou (formerly UCB)*
 - *Bruce Kutter (UCD)*
 - *Patrick J. Fox (formerly UCSD)*
 - *Jose I. Restrepo (UCSD)*
- *Student researchers*
 - *Grigorios Antonellis (formerly UCB)*
 - *Gabriele Guerrini (formerly UCSD)*
 - *Andrew Sander (UCSD)*
- *Technical staff at NEES @ UC San Diego*
 - *Dan Radulescu*
 - *Paul Greco*
 - *Alex Sherman*
 - *Hector Vicencio*
 - *Raymond Hughey*
 - *Robert Beckley*
 - *Lawton Rodriguez*

